

Planar Sliding

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①

Coulomb frict. at a pt. is well defined.

What if we have a contact patch?

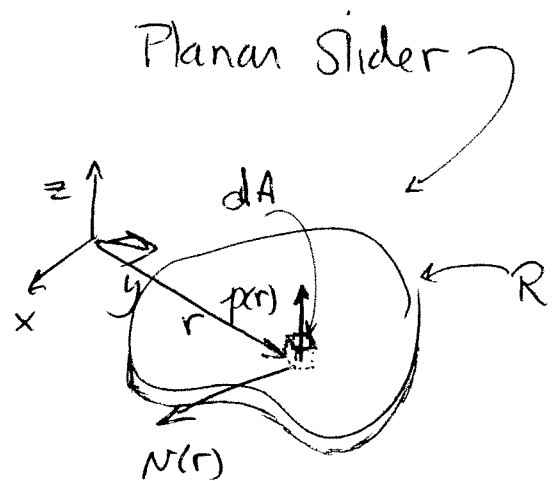
We would like a law like Coulomb's that is "easy" to apply.

Let $\mu =$ coeff. of frict
assume constant

$R =$ contact region

$p(r) =$ pressure

$v(r) =$ velocity



Differential Forces

$$\text{Normal} = p(r) dA$$

$$\text{Friction} = -\mu \frac{v(r)}{\|v(r)\|} p(r) dA, \quad v(r) \neq 0$$

Differential Moments

$$\text{Normal} = r \times p(r) dA$$

$$\text{Friction} = -\mu r \times \frac{v(r)}{\|v(r)\|} p(r) dA, \quad v(r) \neq 0$$

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②

Integrate over R to obtain total forces & moments.

$$f_o = f_n = \int_R p(r) dA$$

$$n_n = -\mu \int_R r \times \frac{\nabla(r)}{\|\nabla(r)\|} p(r) dA$$

$\nabla(r) \neq 0$
in finite patch

$$f_f = -\mu \int_R \frac{\nabla(r)}{\|\nabla(r)\|} p(r) dA$$

"

$$n_f = -\mu \int_R r \times \frac{\nabla(r)}{\|\nabla(r)\|} p(r) dA$$

"

In general, one needs to know $p(r)$, $\nabla(r)$, & R to integrate.

Removing one point from integral where $p(r) dA$ is finite does not change \int_R .

Consider two cases:

- 1.) Translation
- 2.) Rotation about instantant center.

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First define centroid of

$$\bar{r} = \frac{\int_R r p(r) dA}{\int_R p(r) dA}$$

Skip to pages 4,5,6

$$\int_R p(r) dA$$

Case 1: Pure Translational Sliding

$$N(r) = \text{constant}$$

$$f_f = -\mu \frac{N(r)}{\|N(r)\|} \int p(r) dA = \boxed{-\mu \frac{N(r)}{\|N(r)\|} f_n = f_f}$$

$$n_f = -\mu \int_R r p(r) dA \times \frac{N(r)}{\|N(r)\|}$$

$$= \int r p(r) dA \times -\mu \frac{N(r)}{\|N(r)\|} \leftarrow \frac{\int_R r p(r) dA}{\int_R p(r) dA}$$

$$= \frac{\int r p(r) dA}{\int p(r) dA} \times -\mu \frac{N(r)}{\|N(r)\|} \int p(r) dA$$

$$n_f = r_0 \times f_f$$

Skip back to page
(6): rotation

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Center of Friction

④

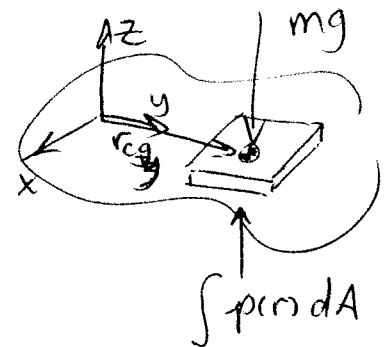
Center of gravity is place where one can lump gravity force, mg .

Would like an analogous point for friction force.

Consider slider at rest on plane.

$$m\ddot{z} = \int p(r) dA - mg = 0$$

$$\boxed{\int p(r) dA = mg}$$



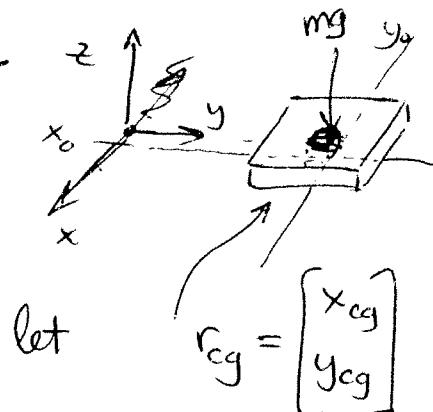
Centroid of Pressure Distribution is point about which ~~the~~ moments applied by pressure distrib are zero.

Find (x_0, y_0) w/ no moment

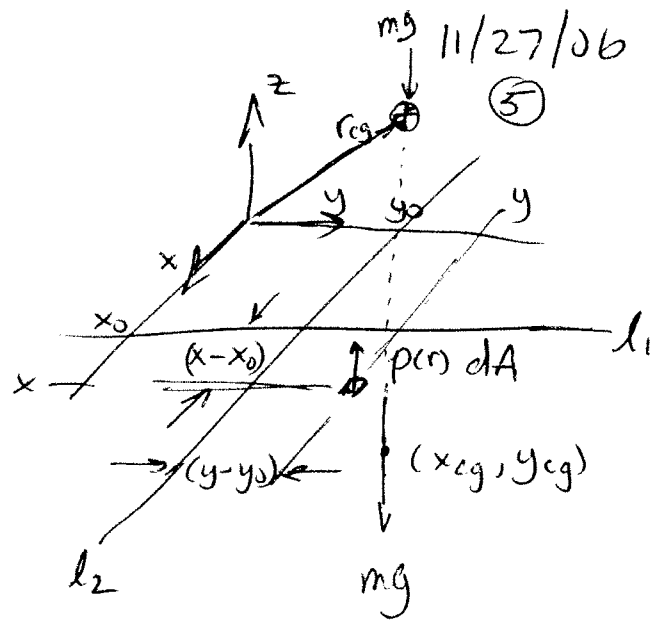
~~$$\int_R (y - y_0) p(r) dA = mg \& r_{cg} = 0$$~~

~~$$\int_R (x - x_0) p(r) dA$$~~

(see next page)



Sum of moments about
lines \parallel to x-axis \perp y-axis
equal zero



Mom. about $l_1 = 0$

$$(x_{cg} - x_0)mg + \int_R -(x - x_0) p(r) dA = 0$$

$$x_{cg}mg - x_0mg - \int_R x p(r) dA + \underbrace{\int_R x_0 p(r) dA}_{x_0 mg} = 0$$

x_0 is constant

$$\frac{x_{cg}mg}{mg} = \frac{\int_R x p(r) dA}{mg = f_n}$$

$$\therefore x_{cg} = x_0 \quad (\text{Note: } \frac{\int_R x p(r) dA}{\int p(r) dA} = x_0 \text{ by def.})$$

\therefore Under non-accelerating planar motion

$$\begin{bmatrix} x_0 \\ y_0 \end{bmatrix} = \begin{bmatrix} x_{cg} \\ y_{cg} \end{bmatrix}$$

\therefore Center of friction is projection
of center of mass to plane of
sliding.

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Center of Friction allows other forces
as long as they are in the support plane, since
then they don't alter the preceding moment sums. (6)

Case 2: Rotation

Suppose body is rotating about
a point r_{IC}

$$\begin{aligned} v(r) &= \omega \times (r - r_{IC}) \\ &= \hat{k} \dot{\theta} \times (r - r_{IC}) \end{aligned}$$

sliding direction at r is ...

$$\frac{v(r)}{\|v(r)\|} = \text{sgn}(\dot{\theta}) \hat{k} \times \frac{r - r_{IC}}{\|r - r_{IC}\|}$$

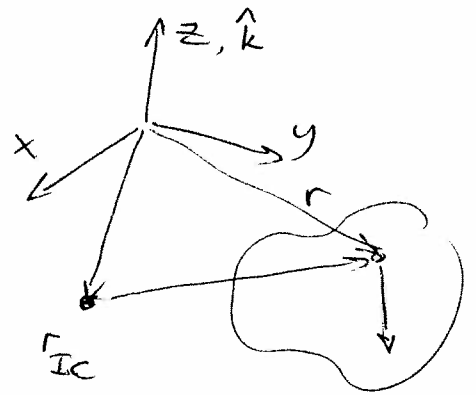
Substituting into defs of page (2) gives

$$f_f = -\mu \text{sgn}(\dot{\theta}) \hat{k} \times \int_R \frac{r - r_{IC}}{\|r - r_{IC}\|} p(r) dA$$

$$(n_f)_z = -\mu \text{sgn}(\dot{\theta}) \int r \cdot \frac{r - r_{IC}}{\|r - r_{IC}\|} p(r) dA$$

Skip back to
page 3

Case 1:



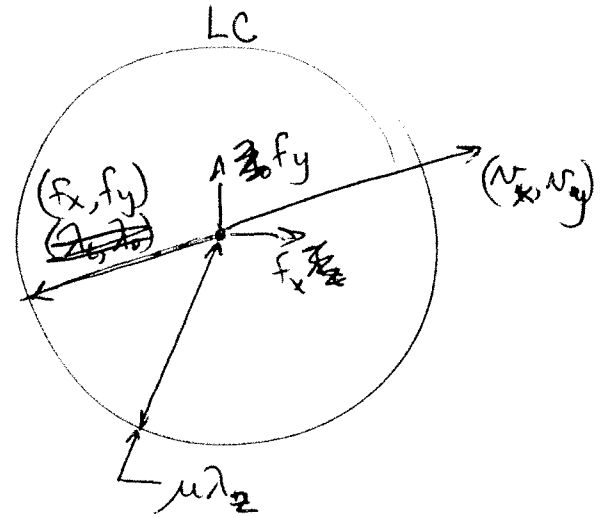
Limit Surfaces & Curves

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Consider a point slider in the plane

For a given normal force, (N_x, N_y) , the limit curve, LC, contains all possible friction forces



Friction force is one that dissipates maximum power

$$(\bar{f}_x, \bar{f}_y) = \operatorname{argmax}_{(f_x, f_y) \in LC} ((f_x, f_y) \cdot (N_x, N_y))$$

Equivalently, (\bar{f}_x, \bar{f}_y) satisfies:

$$[(\bar{f}_x, \bar{f}_y) - (f_x, f_y)^*] \cdot (N_x, N_y) \geq 0$$

~~$(f_x, f_y)^* \in LC \cup \dots$~~
 ~~$\dots \text{Int } LC$~~

$$\forall (f_x, f_y)^* \in \mathcal{F}$$

where $\mathcal{F} = LC \cup \text{Int}(LC)$

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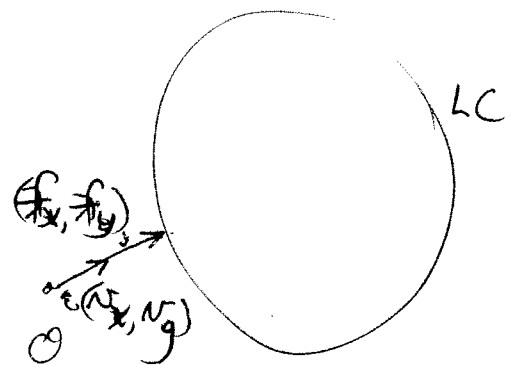
(8)

Notice that:

$(f_x, f_y) \perp LC$ when $(v_x, v_y) \neq 0$!

$(f_x, f_y) = (0, 0)$ is interior to LC

otherwise friction could generate energy



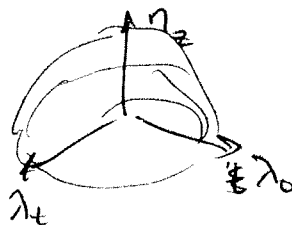
We want more graphical techniques - for planar sliding.

We would like to extend this idea to contact regions.

would like LS (limit surface) to contain all possible friction wrenches.

would like to retain property that $(v_x, v_y) \perp LS$!

Goyal Cornell Phd 1989 did this extension



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Here are the properties of LS's.

If $p(x)$ is finite everywhere (no concentrated points of force), the LS is strictly convex

and each mapping between $(f_x, f_y) \neq (n_x, n_y)$ is 1-1 onto if $(n_x, n_y) \neq 0$.

~~(z, z_0)~~ ~~(n_x, n_y)~~

If $p(x)$ contains discrete points of support, then LS contains flat facets.

~~If $p(x)$ is~~

well defined

~~where~~ LS has a normal, ~~(z, z_0)~~ is the friction force is on LS ~~is~~ such

that the normal to LS is ~~is~~ $\parallel [E(n_x, n_y)]$.

The projection of the LS onto the (z, z_0) plane is the circle of radius

LS contains the origin

LS is symmetric wrt the (f_x, f_y) -plane.

Example: 1 point of support

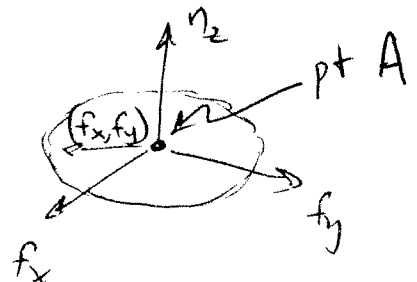
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~~First~~. What is LS for a single point.

Origin at contact point. $n_z = 0$

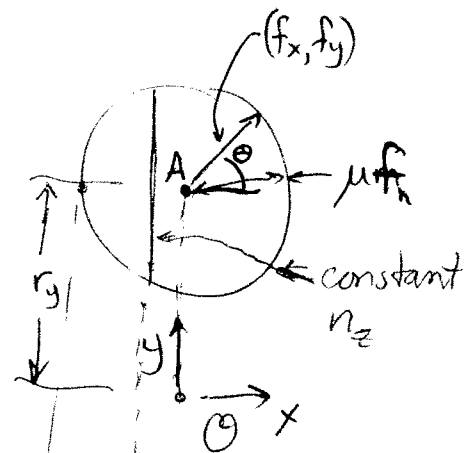
$$\text{wrench} \triangleq w = \begin{bmatrix} f_x \\ f_y \\ n_z \end{bmatrix}$$



Origin at ~~contact~~ point not equal to contact point

$$n_z = (r \times f)_z$$

$$r = \begin{bmatrix} 0 \\ r_y \\ 0 \end{bmatrix} \quad f = \begin{bmatrix} \mu f_n \cos \theta \\ \mu f_n \sin \theta \\ 0 \end{bmatrix}$$

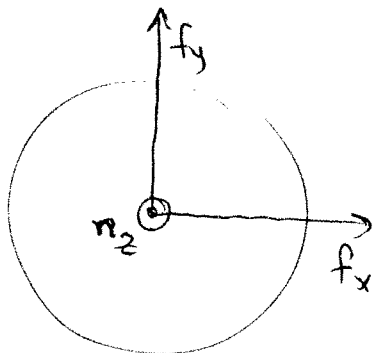


$$n_z = -r_y f_x$$

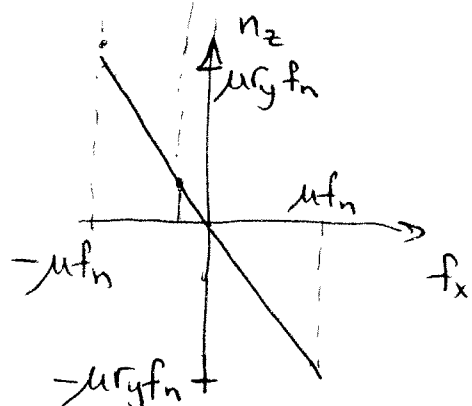
moment is linear in f_x

i	j	k
0	r_y	0
f_x	f_y	0

What is the limit surface?



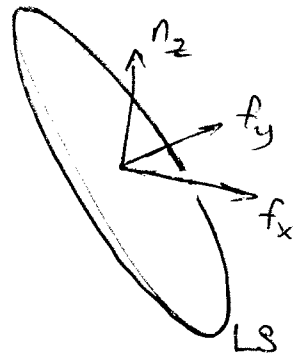
Tilted ellipse



Since projection to (f_x, f_y) plane is a circle

And since n_z varies linearly with f_x ,

The Limit Surface is an elliptical disk containing the origin. \perp the f_y axis



Recall that twists \perp wrenches map forces, torques, velocities, \perp ang vels. to the origin!

Where is a twist, frict force pair?
That maximizes dissipation?

Let twist be rotation in positive sense about origin

$$W^T = \begin{bmatrix} N_x \\ N_y \\ \omega_z \end{bmatrix}$$

$$N_x = N_y = 0 \quad \omega_z > 0$$

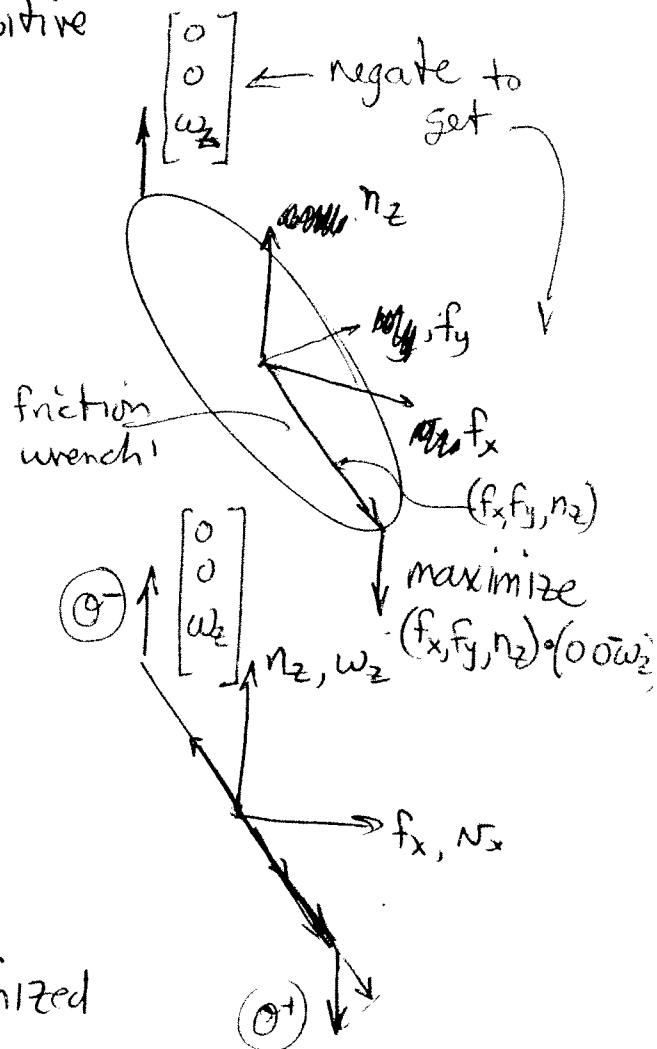


maximize power dissipation.

$$\max (f_x, f_y, n_z) \cdot (N_x, N_y, \omega_z) = -v^T W w$$

Project ^{negative} twist into the space of the Limit Surface. Then find location where

$(-\text{twist} \cdot \text{frict wrench})$ is maximized



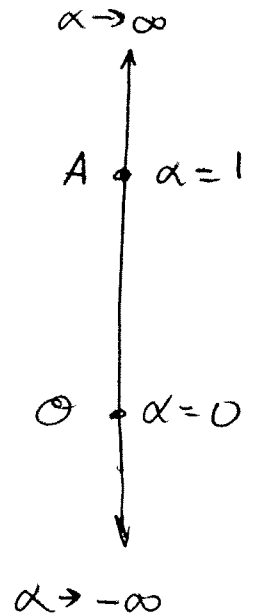
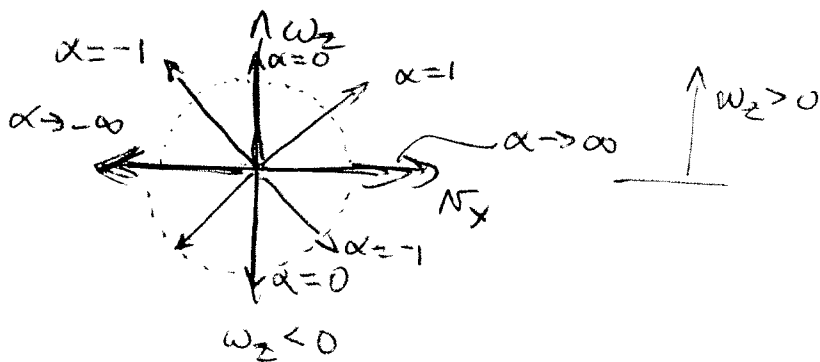
Consider all IC's along line
containing $A \notin \mathcal{O}$.

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(11.1)

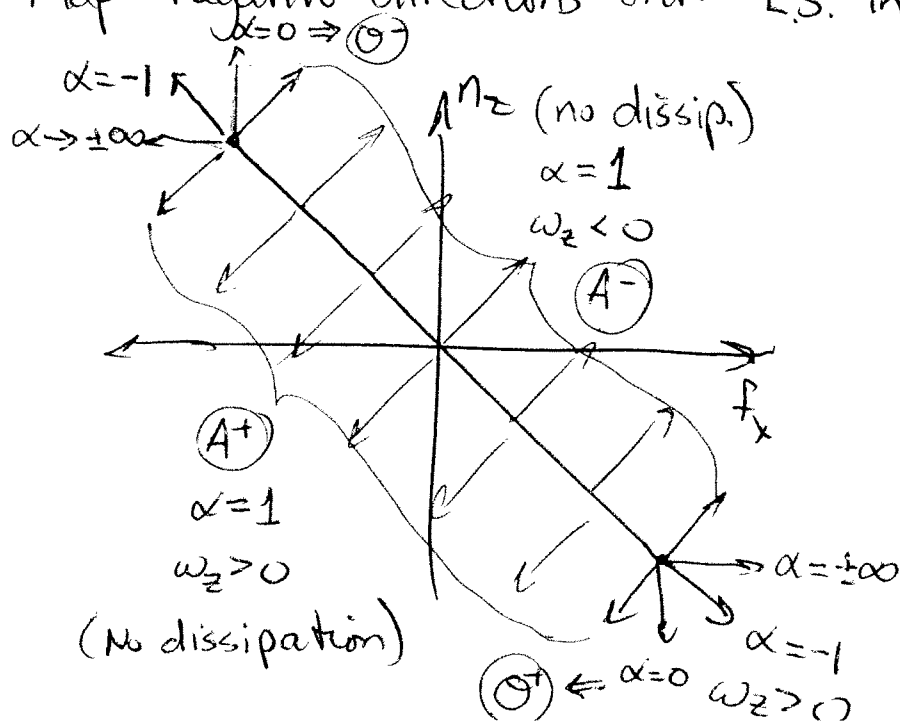
$$IC = \alpha A + (1-\alpha)\mathcal{O}^{\circ}; \quad -\infty < \alpha < \infty$$

Plot all possible twists
for these IC's



All directions in (N_x, w_z) plane are possible.

Map negative directions onto L.S. in wrench space



$\alpha = 1$
Many wrenches
for 1 twist

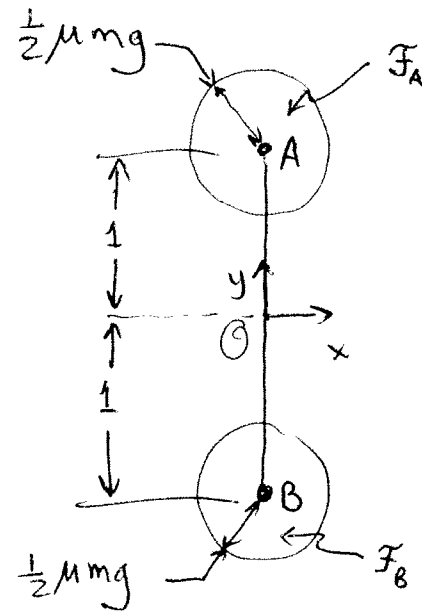
$\alpha \neq 1$
Many twists give
1 wrench

Example: Two Points of Support

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Assume weight is evenly distributed



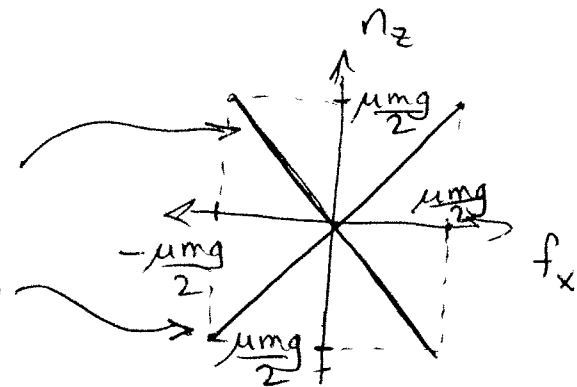
The L.S. contains all possible wrenches.

What does it look like?

Edge view

Ellipse from contact A

Ellipse from contact B



The L.S. contains all

wrenches from $\mathcal{O}A \neq \mathcal{O}B$,

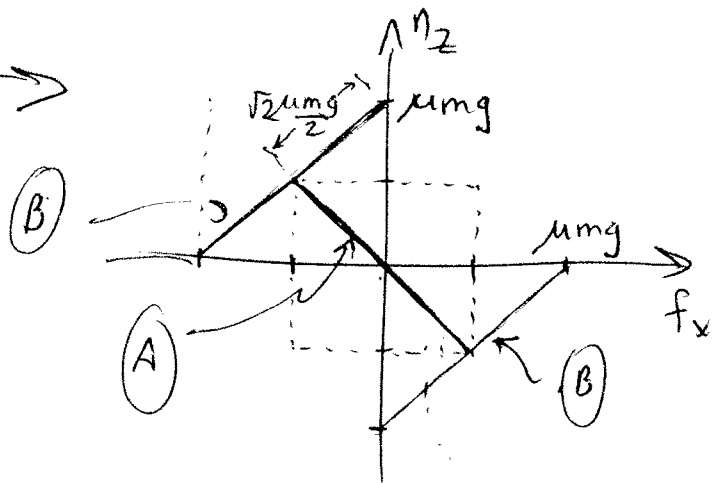
i.e. the ~~M~~ Minkowski sum of wrenches from the two ellipses.

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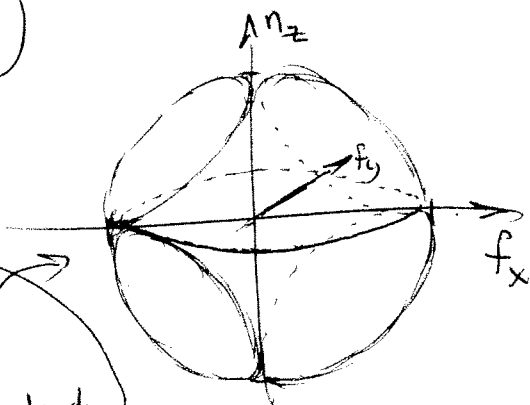
Fix (A).

Slide (B) along



Fix (B)

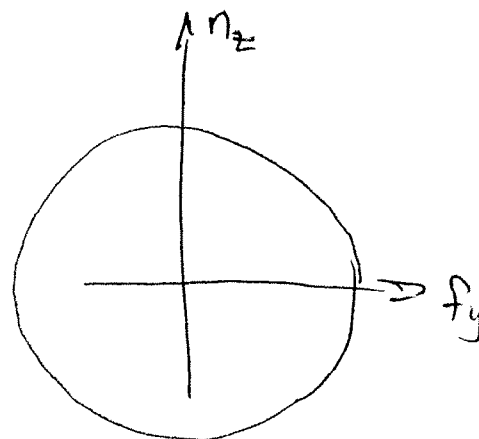
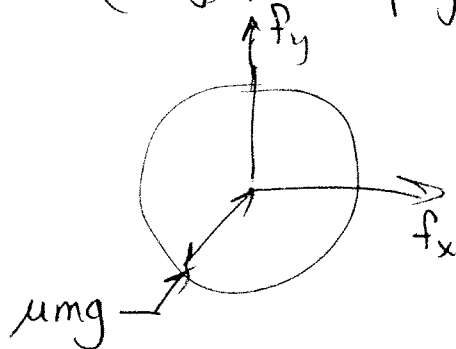
Slide (A)



See figure 6.15 on pg 138 of text

(f_y, n_z) plane projection

(f_x, f_y) plane projection



Text claims that cross-section of LS. in (f_y, n_z) plane is a circle. I don't see it!

Must be non-circular cross-sections as you rotate about n_z / f_y . Then LS is a sphere minus 4 flat ~~solid~~ chords!..

No. Then elliptical facets would be circular!

Look at Space of possible
rotations about line thru $O \neq A$

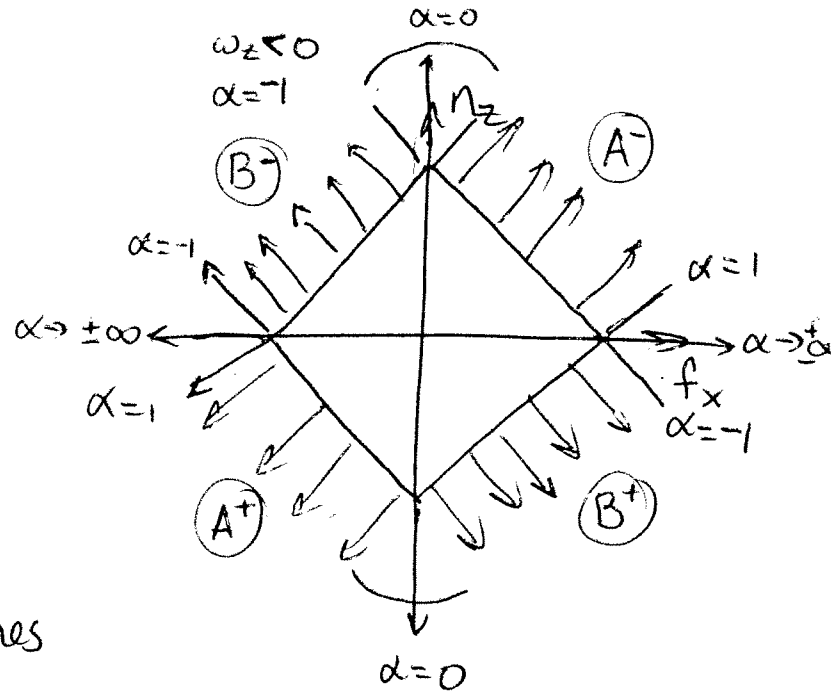
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Same twist plot
as before.

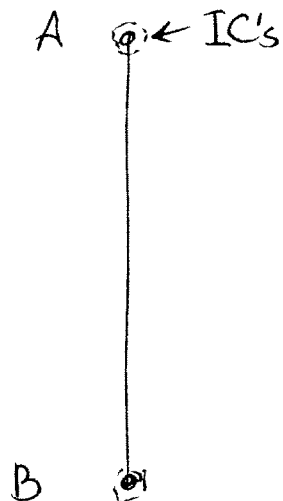
Map onto L.S.

As expected
Rotation about A or B
gives many possible wrenches



Edges of Elliptical Facets

correspond to IC's infinitesimally
close to B or A.

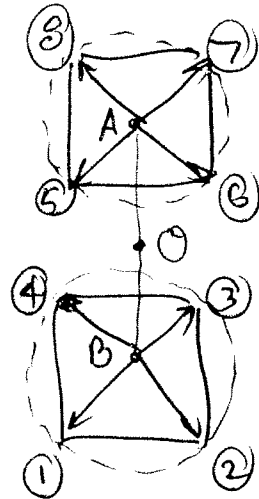


Relate to $W_f \lambda_f, \lambda_f \geq 0$

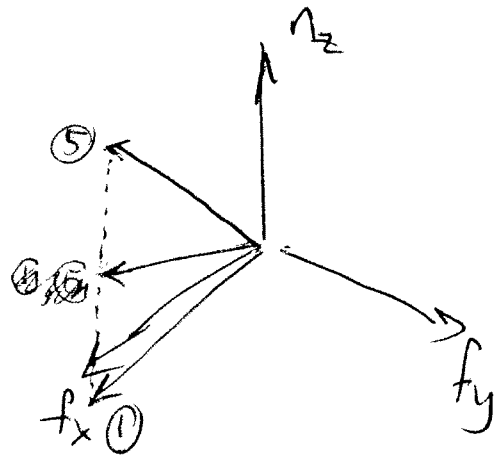
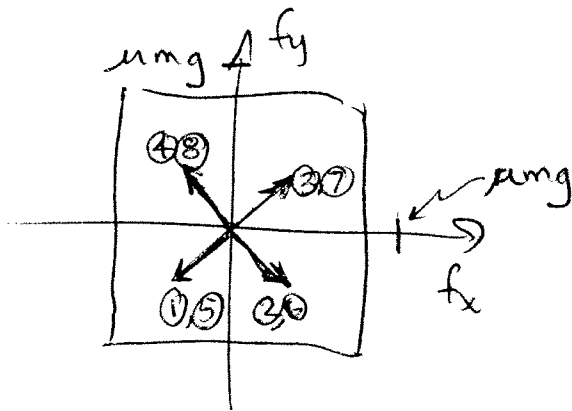
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(15)

4 frict directions
per contact



L.S. becomes a
polyhedron with 8 vertices.



Note that all
moments are
the same in
magnitude.

$W_f \lambda_f, \lambda_f \geq 0$ is a
representation of Minkowski
sum of individual frict cones

\therefore new LS is a cube
inside LS from
Coulumb model with
8 vertices on surface.