

## 4.3.1: Def of Basic MP. Problem

configuration space

World

$$W = \mathbb{R}^2 \text{ or } \mathbb{R}^3$$

Obstacle region

$$\mathcal{O} \subset W$$

a.k.a. "impermissible" region

Robot

$$A \subset W$$

Assume  $A \neq \emptyset$  are expressed as semi-algebraic models

Let  $q \in C$  be a configuration of the robot  $A$ .

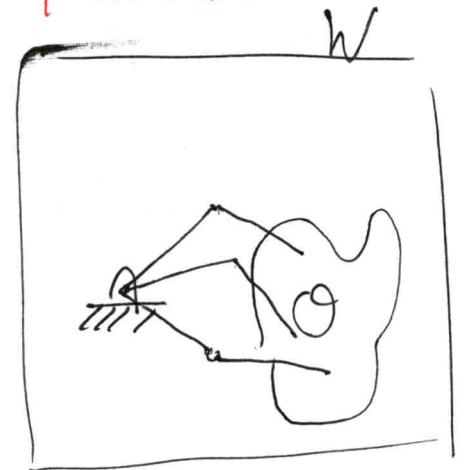
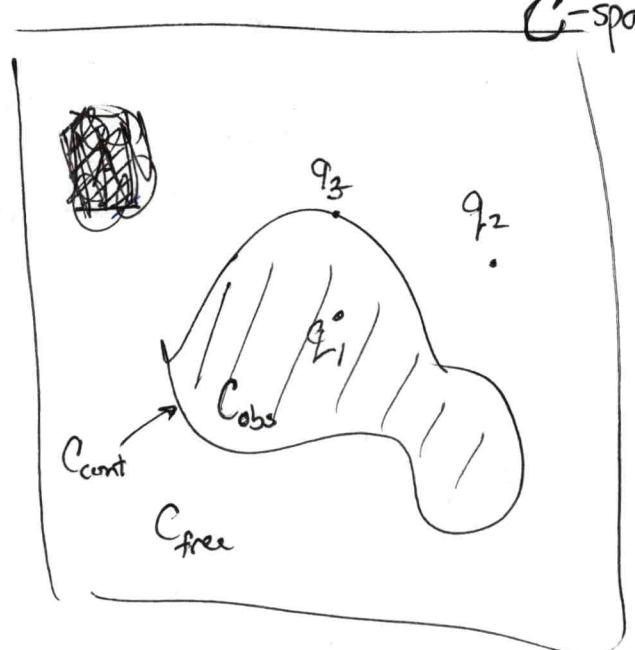
$$\text{In } W = \mathbb{R}^2, q = (x_t, y_t, \theta)$$

$$\text{In } W = \mathbb{R}^3, q = (x_t, y_t, z_t, h)$$

$\leftarrow$  unit quaternion

The obstacle region mapped into  $C$ -space

$$C_{\text{obs}} = \{q \in C \mid A(q) \cap \mathcal{O} \neq \emptyset\}$$



2/11/18

②

$$C_{\text{free}} = C \setminus C_{\text{obs}}$$

$$= \{q \in C \mid A(q) \cap O = \emptyset\}$$

$$\text{cl}(O) \cap \text{cl}(A(q))$$

$$C_{\text{cont}} = \{q \in C \mid \text{int}(O) \cap \text{int}(A(q)) = \emptyset \text{ AND } O \cap A(q) \neq \emptyset\}$$

interior  
of a set



Motion Planning  
Problem general  
Formulation 4.1

① Given  $W = \mathbb{R}^n$  ( $n=2$  or  $3$ ),  $O$ ,  $A$ .

②  $C$ ,  $C_{\text{obs}}$ , &  $C_{\text{free}}$  are implicitly derived

③ Initial & goal configs are given  $q_I, q_G \in C_{\text{free}}$

a.k.a. a planning query.

④ A planning alg computes a continuous path

$\tau: [0, 1] \rightarrow C_{\text{free}}$  such that  $\tau(0) = q_I$  and  $\tau(1) = q_G$ ,

OR correctly report that a path does not exist,

1980's  
or 1990's Reif showed that this problem is PSPACE-hard  
which implies NP-hard!

## LaValle\_Ch4-3

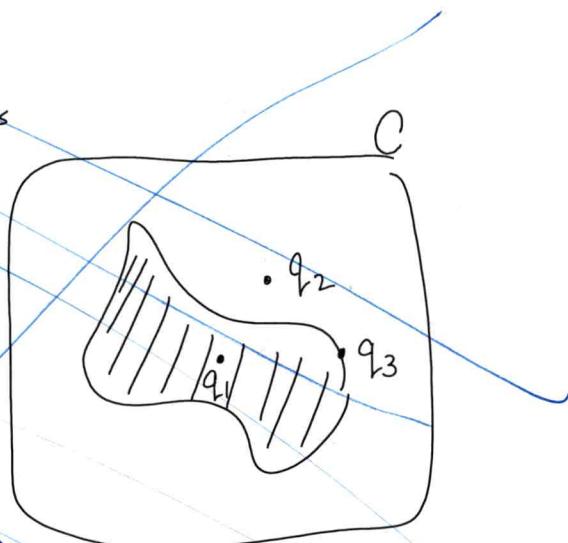
Monday, April 09, 2012

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### 4.3 The C-space Obstacle, $C_{\text{obs}}$

Let  $q \in C$  denote  
a config. of the robot

Let  $A(q)$  be the robot  
in config  $q$ .



$$C_{\text{obs}} = \{q \in C \mid A(q) \cap \text{Int}(\mathcal{O}) \neq \emptyset\}$$

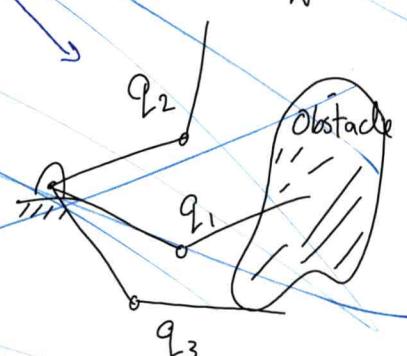
$$C_{\text{cont}} = \{q \in C \mid A(q) \cap \mathcal{O} \neq \emptyset, \\ A(q) \cap \partial \mathcal{O} = \emptyset\}$$

equivalently,

$$C_{\text{cont}} = \partial C_{\text{obs}}$$

$$C_{\text{free}} = C \setminus (C_{\text{obs}} \cup C_{\text{cont}}) = C \setminus \text{cl}(C_{\text{obs}})$$

↑ closure of a set



### 4.3.2 Explicit representations of $C_{\text{cont}} = \partial C_{\text{obs}}$

(LaValle treats  $C_{\text{obs}}$  and  $C_{\text{obs}} \cup C_{\text{cont}}$ ) =  $\text{cl}(C_{\text{obs}})$

Definition: Minkowski difference of two sets in  $\mathbb{R}^n$

$$X \ominus Y = \{x - y \in \mathbb{R}^n \mid x \in X, y \in Y\}$$

Each set has a  
reference frame

$$X \ominus Y = \{x - y \in \mathbb{R}^n \mid x \in X, y \in Y\}$$

↑ vector subtraction

then it has a reference frame embedded in it.

Definition: Minkowski sum

$$X \oplus Y = \{x + y \in \mathbb{R}^n \mid x \in X, y \in Y\}$$

↑ vector addition

Note:  $X \ominus Y = X \oplus (-Y)$  where  $-Y$  is the set of negated elements of  $Y$ .

Example in  $\mathbb{R}^2$

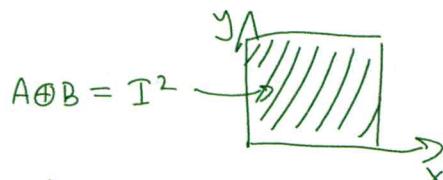
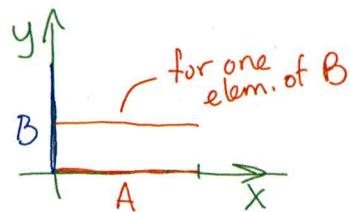
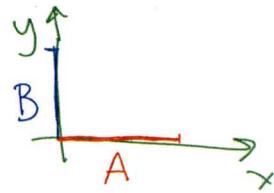
Let  $A = I = ([0, 1], 0)$  = interval on x-axis

$B = I = (0, [0, 1])$  = interval on y-axis

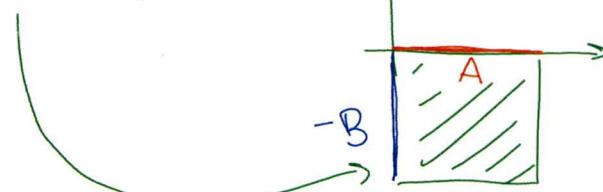
What is  $A \oplus B$ ?

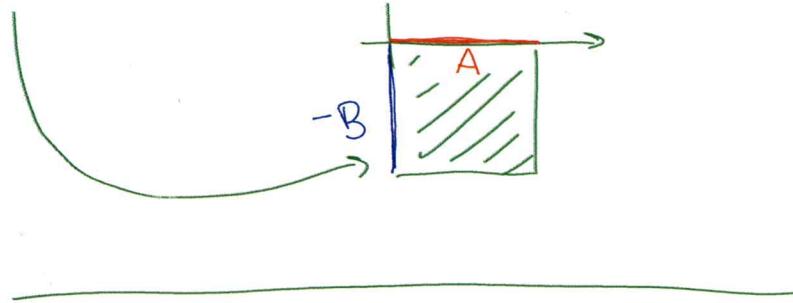
Add every element of  $A$

to every element of  $B$



$A \ominus B = ? \rightarrow$



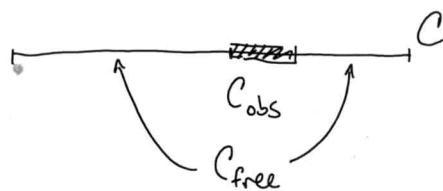
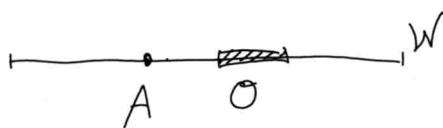


Using  $\theta$  to determine  $C_{free}$  &  $C_{obs}$

Simplest case: A is a particle.

It can be reasonable to treat robot as a point, if features in World are much larger than robot.

1D world

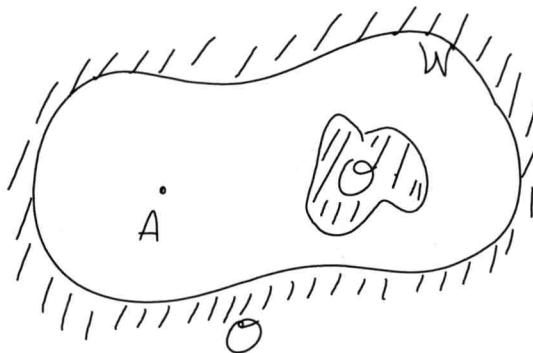


2D world

$$\text{Again } C_{obs} = \text{Int}(\theta)$$

$$C_{cont} = \partial \theta$$

$$C_{free} = W \setminus cl(\theta)$$



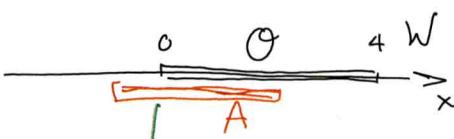
Same for 3D worlds

Robots of finite extent:

1D:

$$\text{Let } A = [-1, 2]$$

$$\mathcal{O} = [0, 4]$$



To create  $C_{\text{obs}}$ ,  $C_{\text{cont}}$ ,  $C_{\text{free}}$ ,

we need a ref. pt. on A.

(Choose the zero point)

$C$  represents possible positions of A by possible positions of the ref. point.

Create the  $C_{\text{obs}}$  by negating A, then placing the ref. point at every point in  $\mathcal{O}$ . Perform union of all placed copies of  $-A$ .

$$\text{cl}(C_{\text{obs}}) = \mathcal{O} \oplus -A = [0, 4] \oplus [-2, 1] = \begin{matrix} 0 & 1 & \dots & 4 \\ \downarrow & \downarrow & & \downarrow \\ [-2, 1] \cup [-1, 2] \cup [2, 5] \end{matrix}$$
$$\text{cl}(C_{\text{obs}}) = [-2, 5]$$
$$C_{\text{obs}} = \{x \mid -2 \leq x \leq 5\}$$

Alternative view: place  $A(q)$  at every  $q$  where  $A \neq \emptyset$  overlap or touch. The union of the ref pt locations is the  $C_{\text{obs}}$ .

$$C_{\text{free}} = \{x \mid x < -2 \vee x > 5\}$$

$$C_{\text{cont}} = \{x \mid x = -2 \vee x = 5\} \quad \text{just touching}$$

Why do we define  $C_{\text{obs}}$  by  $\emptyset \oplus (-A)$  instead of  $\emptyset \oplus A$ ?

Consider 1D case:

Write the non-collision constraint for the left side of  $\emptyset$ :

position of pt on robot relative to ref pt.

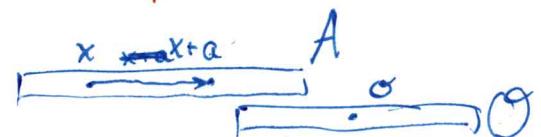
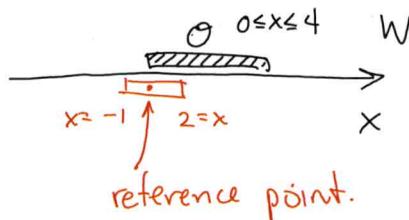
position of ref pt in  $W$

$x + a < \emptyset, \forall a \in A(x), \forall \emptyset \in \emptyset$

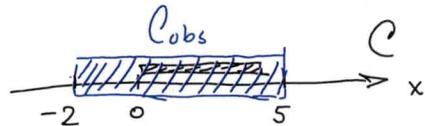
point on obstacle in  $W$

$\Rightarrow x < \emptyset - a, \forall a \in A(x), \forall \emptyset \in \emptyset$

This is Definition of Minkowski difference



Worst case:  $x < -2$

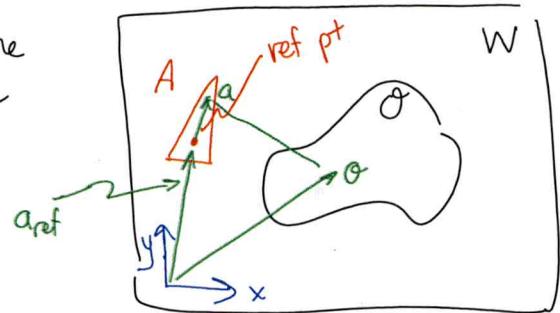


You can apply on right also

$$x > \emptyset - a, \forall a \in A, \forall \emptyset \in \emptyset$$

worst case:  $x > 5$

2D example works the same way, but constraints are more complicated



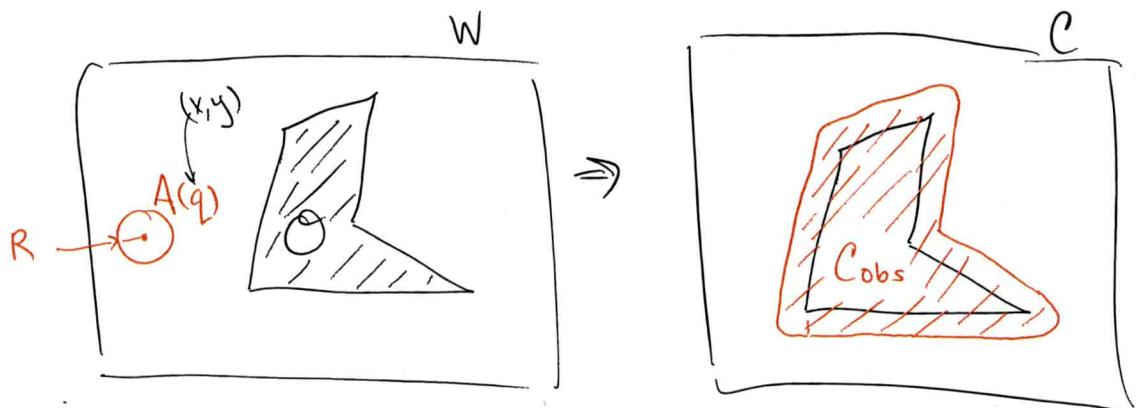
pt on robot,  $\eta$

$$\eta = a_{\text{ref}} + a, \quad a \in A(\eta)$$

$q \in C_{\text{obs}}$  if  $a_{\text{ref}} + a = \theta$  for some  $\theta \in \Theta$   
 for some  $a \in A$

$q \notin C_{\text{obs}}$  if  $a_{\text{ref}} \neq \theta - a, \forall a \in A(q), \forall \theta \in \Theta$   
 Minkowski difference

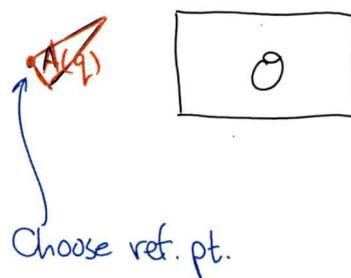
Disc robot  $\leftarrow$  Minkowski sum = Minkowski difference



Planar Translation Only Robot.

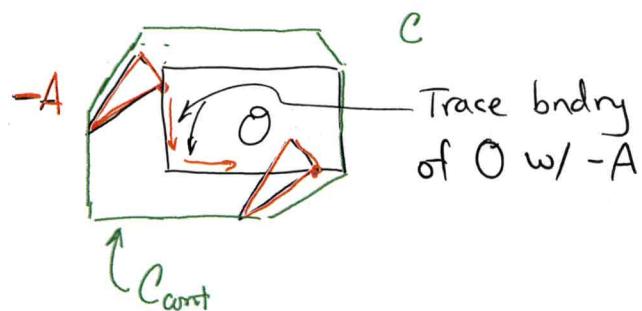
$C_{\text{free}}$  is set of  
positions of ref.

point  $\exists A \cap \Theta = \emptyset$



$$\text{cl}(\mathcal{C}_{\text{obs}}) = \mathcal{O} \oplus -A$$

Add  $-A$  to every point in  $\mathcal{O}$



Skip to next page - star alg.

David Hsu's slides have a few nice pictures & animations.

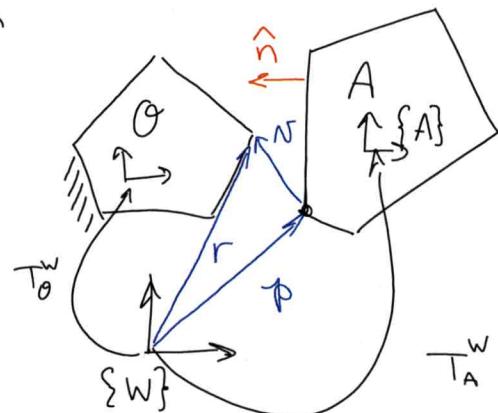
Formulas for the boundary of  $\mathcal{C}_{\text{obs}}$

for planar world with

$\mathcal{O}$  &  $A$  defined as polygons

Show  
Brost  
Figure

EV Contact - edge of robot in contact with vertex of  $\mathcal{O}$ .



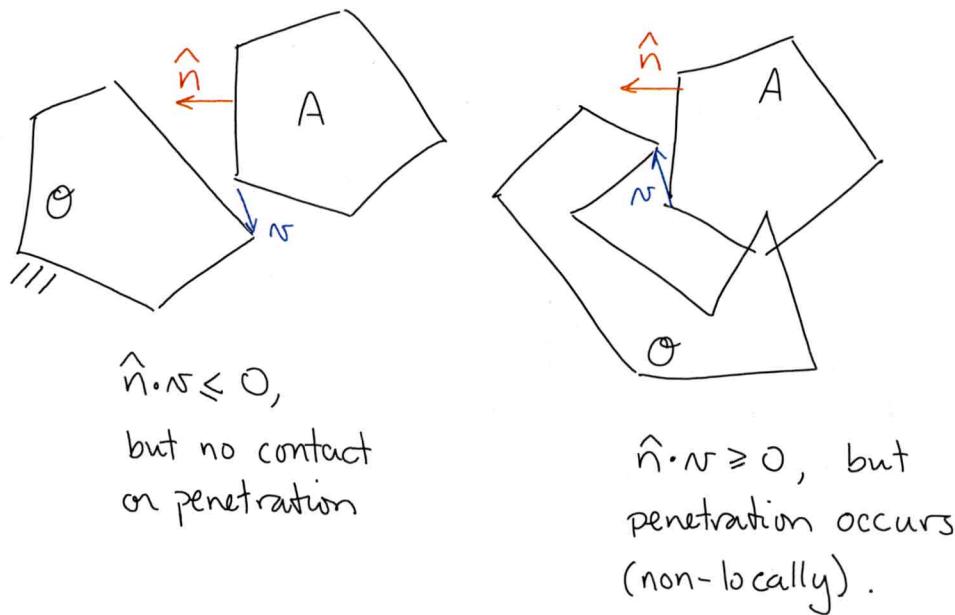
$$\hat{n} \cdot N = 0 \quad \text{potential contact}$$

$$\hat{n} \cdot N < 0 \quad \text{potential penetration}$$

$$\hat{n} \cdot N > 0 \quad \text{local separation}$$

$$N = r - p$$

Why the qualifiers?



To obtain manifold of a given facet, write

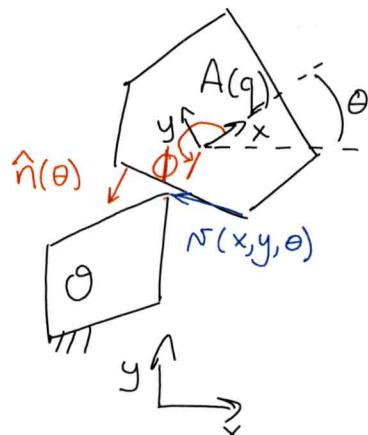
Contact condition as a function of  $q = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}$

Necessary condition  
for contact:

$$\hat{n}(\theta) \cdot N(x, y, \theta) = 0$$

Let  $\phi$  denote the  
angle from the body-fixed  
x-axis to the normal  
direction

$$\hat{n}(\theta) = \begin{bmatrix} \cos(\phi + \theta) \\ \sin(\phi + \theta) \end{bmatrix}$$



Let body-fixed  
frame be  $\{A\}$

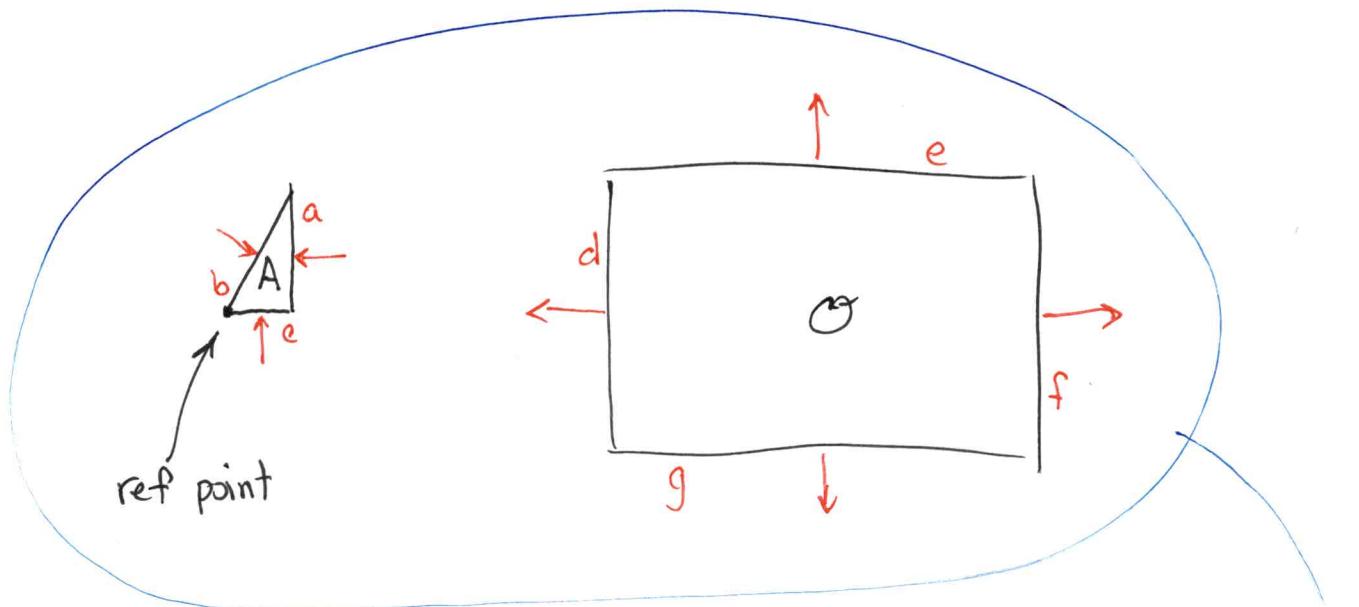
- position of  $\theta$  in

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③

## Star Alg for making C-space obstacles

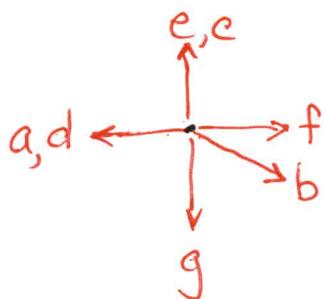
in C-spaces with polygonal bodies w/o rotation.



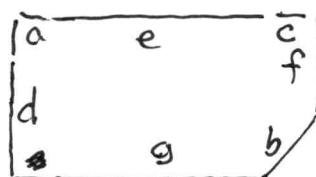
The Cobs can be constructed by laying down the edges of  $A \cup O$  in order of face normals

Easiest w/ ref pt on bndry

- ① Translate A so ref pt touches edge of  $O$  w/o overlap.  
Keep that edge in Cobs.



- ② Walk list of sorted normals  
placing that edge onto current end of Cobs



$$r^w = r^w - p^w = r^w - {}^w_T_A p^A$$

position of  $p$  in  
frame A

$${}^w_T_A = \begin{bmatrix} c_\theta & -s_\theta & x \\ s_\theta & c_\theta & y \\ 0 & 0 & 1 \end{bmatrix} \in SE(2)$$

$$N(x, y, \theta) = \begin{bmatrix} r_x - c_\theta p_x^A + s_\theta p_y^A - x \\ r_y - s_\theta p_x^A - c_\theta p_y^A - y \end{bmatrix}$$

position of  
obstacle  
vertex in W

position of  
origin  
of robot frame in W

Substitute into  $\hat{n}(\theta) \cdot N(x, y, \theta) = 0$

$$0 = \cos(\theta + \phi)[r_x - c_\theta p_x^A + s_\theta p_y^A - x] + \sin(\theta + \phi)[r_y - s_\theta p_x^A - c_\theta p_y^A - y]$$

(This eq. defines a 2D "variety" in 3D C-space  $(x, y, \theta)$ ).

Nonlinear trigonometric polynomial in  $\theta$   
(e.g.,  $\cos(\theta + \phi) \cdot \cos(\theta)$ )

Linear in  $(x, y)$  ..... This is why Cobs has linear surfaces  
for fixed orientations of A.

$$\boxed{ax + by + c = 0}$$

where  $a = -\cos(\theta + \phi)$ ,  $b = -\sin(\theta + \phi)$ ,

$$\text{and } c = \cos(\theta + \phi)[r_x - c_\theta p_x^A + s_\theta p_y^A] \\ + \sin(\theta + \phi)[r_y - s_\theta p_x^A - c_\theta p_y^A]$$

Setting this contact eq. = 0 yields a 2D manifold in a 3D space  $(\mathbb{R}^2 \times S^1) = SE(2)$

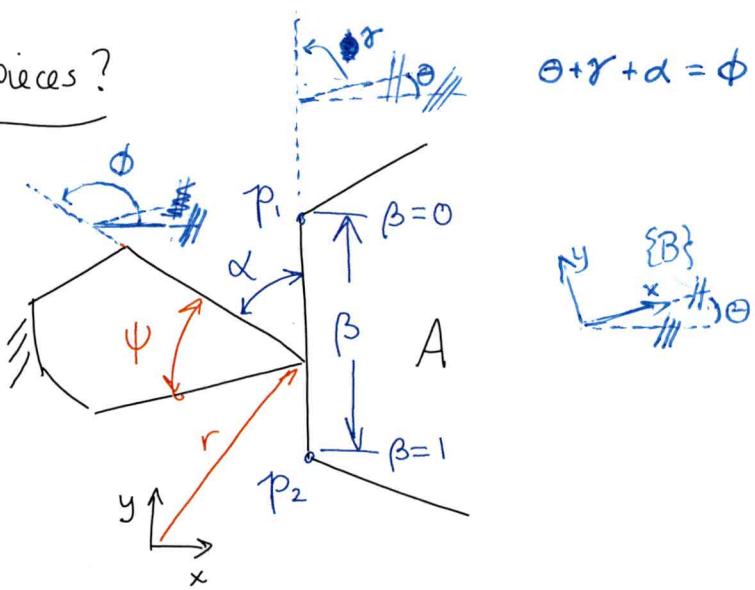
Pieces of this manifold appear in Brost's Cobs

How do we get the pieces?

Another useful formulation ...

$$0 \leq \alpha \leq \pi - \psi$$

$$0 \leq \beta \leq 1$$



r must be on the line segment  $\overline{P_1 P_2}$

$$\begin{bmatrix} p_i^w \\ p_i^y \\ 1 \end{bmatrix} = \begin{bmatrix} c_\theta & -s_\theta & x \\ s_\theta & c_\theta & y \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} p_i^A \\ p_i^y \\ 1 \end{bmatrix}$$

$$i = 1, 2$$

given in geom. model

Substitute  $p_i^w, p_i^y$

into:

$$(1-\beta)p_1^w(x, y, \theta) + \beta p_2^w(x, y, \theta) = r$$

$$0 \leq \beta \leq 1$$

$$0 \leq \alpha \leq \pi - \psi$$

$$\leftarrow \alpha = \phi - \gamma - \theta$$

Choose  $\alpha, \beta$  and solve for  $x, y, \theta$  to get a point on Cobs

If A & O are convex, then this is a patch of Cobs

If A or O are nonconvex, then some of this patch may be cut away by nonlocal interpenetrations!

Other contact types.

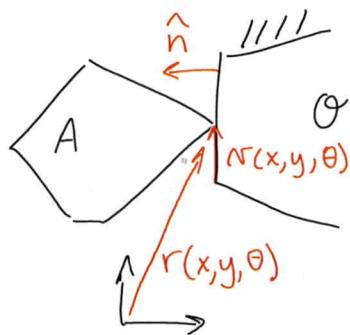
VE contact:

Same procedure, but

$\hat{n}$  is constant

$N$  is  $N(x, y, \theta)$

$r$  is  $r(x, y, \theta)$

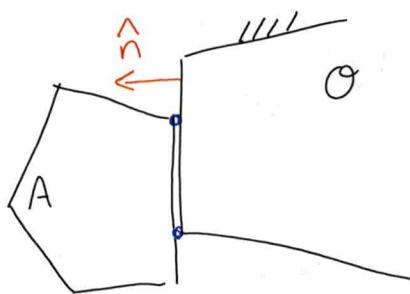


VE  $\Rightarrow$  2D facet of Cobs

EE contact:

Treat as two  
contacts of type

EV or VE



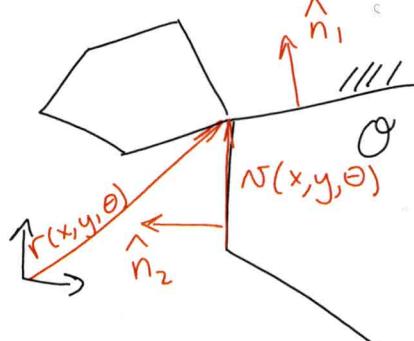
EE  $\Rightarrow$  1D facet of Cobs

However forming equations w/o rotation variable  $\theta$   
makes the equation much easier to solve.

VV contact:

Treat as two  
contacts of type

EV or VE



VV  $\Rightarrow$  1D facet of Cobs

VV contact eq  
gives the points  
on a curved  
facet on Cobs,  
where EV & VE  
facets meet

V... ... at ... (EV EV) m (VF VF) m (F1 X F1)

You can choose (EV, EV) or (VE, VE) or ~~(EV, VE)~~

1 Dof transl  
allowed

doesn't  
always  
work

Simple example of  
a  $C_{obs}$  in  $SE(2)$ .

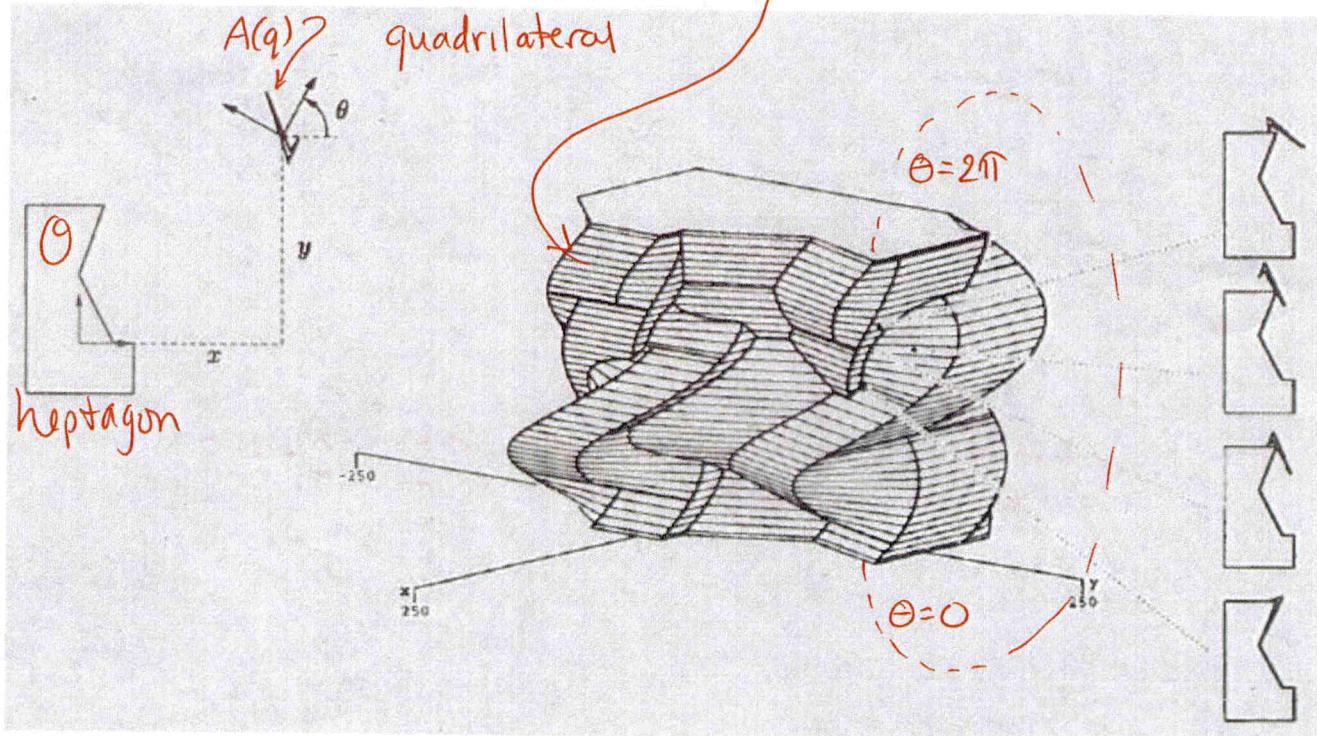
How many  
facets  
are there?

At most:

$$|E_1|=4=|V_1| \Rightarrow 28(E,V) \text{ pairs}$$

$$|E_2|=7=|V_2| \Rightarrow 28(V,E) \text{ pairs}$$

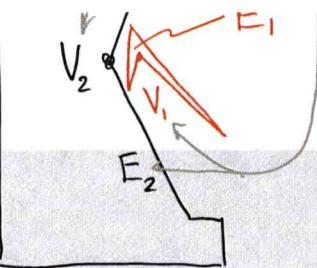
From Randy Brost's Thesis, CS, CMU, 1989.



One infeasible (E, V) pair. There are 8 total.

There are 7 (E, V) infeasible (E, V) pairs.

$$\therefore C_{obs} \text{ has at most } 56 - \frac{13}{2\pi} = 43$$



$\therefore C_{\text{obs}} \text{ has at most } 56 - 13 = 43$   
2D facets?

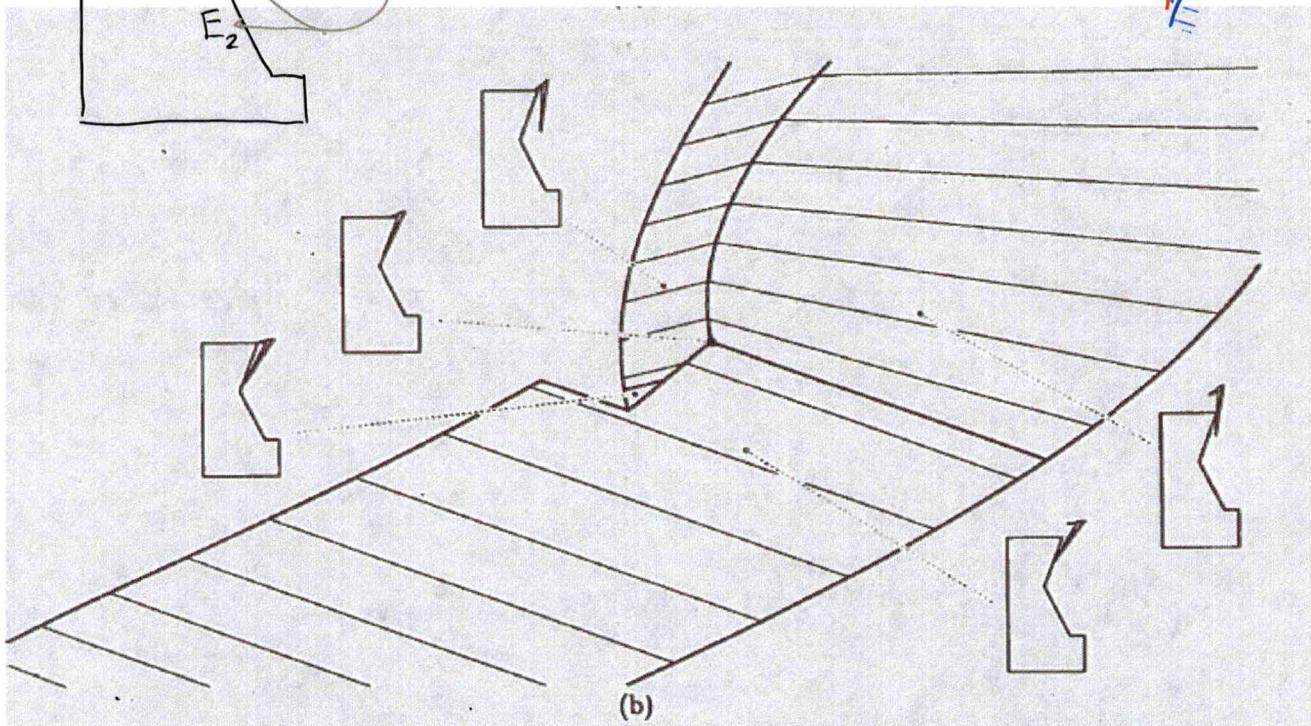
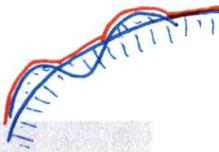


Figure 6: (a) The  $(x, y, \theta)$  configuration-space obstacle of the two polygonal objects.  
(b) An enlarged view of the obstacle features required for the mechanics analysis. The vertex corresponding to the goal configuration is labelled in both (a) and (b).

It's possible that some facets could appear as multiple surface patches, since portions could go under other facets.

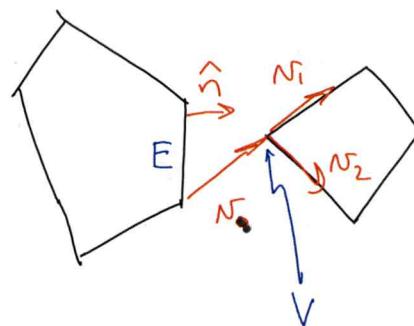
### Collision Checking for Polygons

Assume polygons are convex  
(can partition non-convex ones)

#### Theorem :

A pair of convex polygons are separated iff  $\exists$  a vertex/edge pair  $(E, V) \ni$

$$\hat{n} \cdot n > 0$$



$$\hat{n} \cdot n_1 > 0$$

$$\hat{n} \cdot n_2 > 0$$

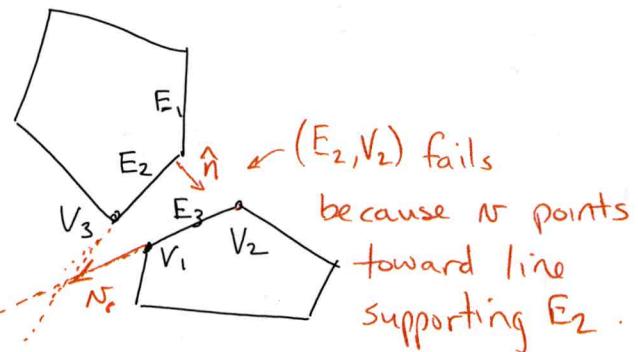
Example:  $\rightarrow$

$(E_1, V_1)$  fails test

$(E_2, V_2)$  fails

$(E_3, V_3)$  succeeds

$(E_2, V_1)$  succeeds too



## Collision Detection for Convex Polygons

$q\_in\_Cfree = \text{false}$

while  $q\_in\_Cfree = \text{false}$

loop over all EV pairs

if  $(\hat{n} \cdot n_1 > 0) \text{ AND } (\hat{n} \cdot n_2 > 0) \text{ AND } (\hat{n} \cdot n) > 0$

$q\_in\_Cfree = \text{true}$

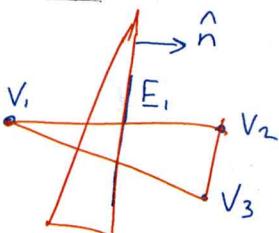
    break

end if

end while

Does this work for this case?

$V_j E_i, i=1,2,3 \\ j=1,2,3 \} \text{ satisfied}$



$$\left. \begin{array}{l} V_j E_i, \quad i=4,5,6 \\ j=4,5,6 \end{array} \right\} \text{satisfied} \quad \text{Yes! It works!}$$

Complexity:

Let  $|V_A|$  &  $|V_O|$  be the numbers of vertices of the robot, A, and the obstacle, O.

For each vertex-edge pair there are 3 inequalities to test  $\Rightarrow O(1)$

There are  $O(|V_A| \cdot |V_O|)$  EV and VE pairs.

$\therefore$  Collision detection is  $O(|V_A| \cdot |V_O|)$

Lavalle's discussion in section 4.3.3 focuses on the negation of the collision-free conditions:

Consider 1 EV pair  $\rightarrow$

$$\text{Let } H_A = H_1 \cup H_2 \cup H_3$$

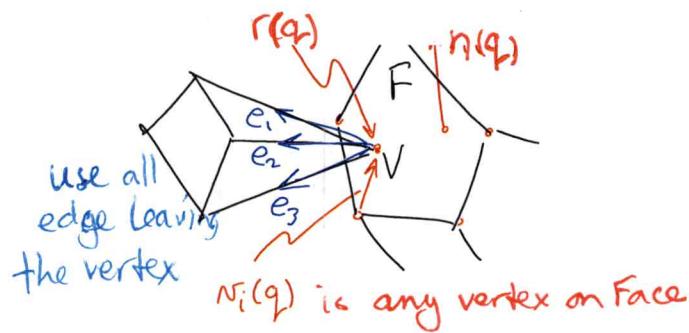
$$\text{where } H_1 = \{q \in C \mid \hat{n} \cdot n_i \leq 0\}$$

negations of previously



What about 3D?

Extension is analogous  
but a bit more  
complicated.



$q \in C_{\text{free}}$  if

$\exists$  a V-F or F-V pair  $\ni$

$$\hat{n} \cdot n > 0$$

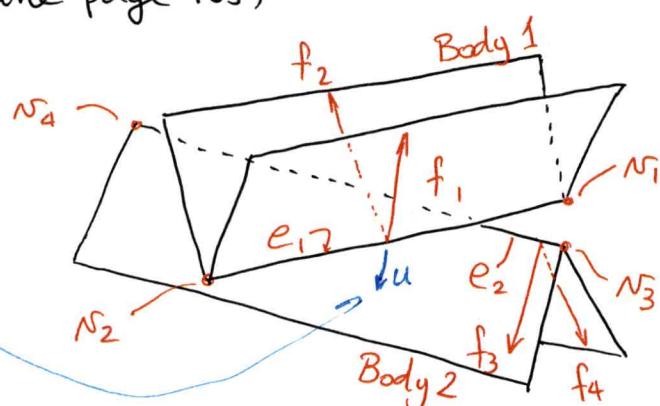
$$\hat{n} \cdot e_i > 0 \quad i = 1, \dots, \# \text{edges}$$

A facet of  $C_{\text{obs}}$  would be defined by  
 $\hat{n} \cdot n = 0$  and  $r(q)$  within the boundaries  
of face  $F$ .

In 3D we have another case, E-E.

(this extends beyond Lavalle page 165)

Let  $u = e_1 \times e_2$   
 $\hat{u} = u / \|u\|$   
 (outward wrt Body 1)



$(n_3 - n_1) \cdot \hat{u} > 0 \Rightarrow e_1 \text{ & } e_2 \text{ are separated}$

$f_1, f_2$  are vectors in faces of Body 1 &  $\perp$  to  $e_1$

$f_1 \cdot \hat{u} \leq 0 \Rightarrow$  no overlap

$f_2 \cdot \hat{u} \leq 0 \Rightarrow$  no overlap

$f_3, f_4$  are vectors in faces of B2 &  $\perp e_2$

$f_3 \cdot \hat{u} > 0 \Rightarrow$  no overlap

$f_4 \cdot \hat{u} > 0 \Rightarrow$  no overlap

### 3D Collision Checking

$q_{\text{in-Cfree}} = \text{false}$

loop over all FV VF EE pairs

while  $q_{\text{in-Cfree}} = \text{false}$

if (separation condition satisfied)

$q_{\text{in-Cfree}} = \text{true}$

    break

end if

end while

Complexity of CD in 3D.

[Latombe '91] It is known that the # of VF, FV, and EE pairs is  $O(|V_A| \cdot |V_o|)$ .

### Fast collision checking - intuition

If relative config does not change much, and polygons were not in collision at previous check, it should be "easy" to find the definitive witness pair.

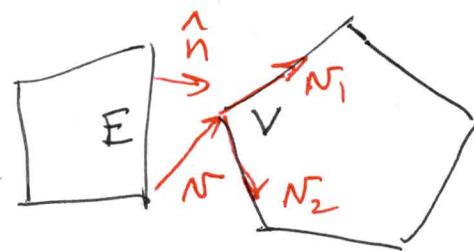
### Section 4.3.3: Explicitly Modeling Cobs

2/12/18  
①

Summary: Use primitives based on negation of the collision-free condition mentioned above.

Consider 2 convex polygons

$$\text{Let } H_A = H_1 \cup H_2 \cup H_3$$



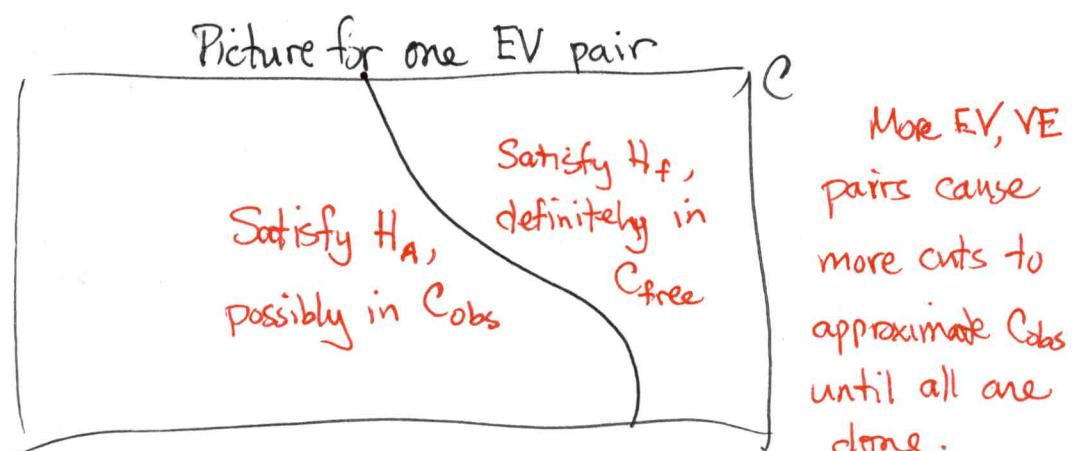
where

$$\left. \begin{aligned} H_1 &= \{q \in C \mid \hat{n} \cdot N_1 \leq 0\} \\ H_2 &= \{q \in C \mid \hat{n} \cdot N_2 \leq 0\} \\ H_3 &= \{q \in C \mid \hat{n} \cdot N < 0\} \end{aligned} \right\}$$

negations of previously defined collision-free conditions

$$C_{\text{free}} = \{q \in C \mid \text{for some EV or VE pair, } (\hat{n} \cdot N_1 > 0 \wedge \hat{n} \cdot N_2 \geq 0 \wedge \hat{n} \cdot N > 0)\}$$

$$C_{\text{obs}} = \{q \in C \mid \text{for all pairs EV \& VE, } (\hat{n} \cdot N_1 < 0 \wedge \hat{n} \cdot N_2 < 0 \wedge \hat{n} \cdot N \leq 0)\}$$



## LaValle Ch4.4 : Closed Kinematic Chains

2/11/18

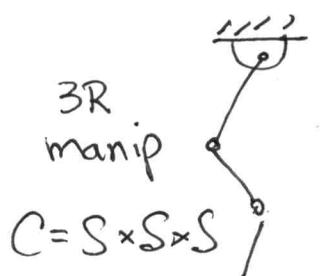
(4)

The C-space of open chains is just the product of C-spaces of each joint

e.g.  $\mathbb{R}^4 \times S^1 \times S^1 \times SE(3)$

The diagram shows a closed kinematic chain consisting of a vertical segment, a horizontal segment, and a curved segment forming a loop. A circular disk labeled "drone" is attached to the vertical segment. Arrows indicate the flow of the chain from the vertical segment through the horizontal and curved segments back to the vertical segment. Brackets with arrows point to different parts of the chain: one bracket points to the vertical segment with the label "drone", another points to the horizontal segment with the label "2 revolute joints", and a third points to the curved segment with the label "four prismatic joints".

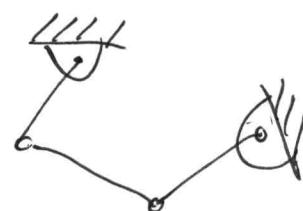
The constraints associated with closing ~~the~~ a loop with kinematic chains, fundamentally changes the structure of C-space.



If joint limits exist,

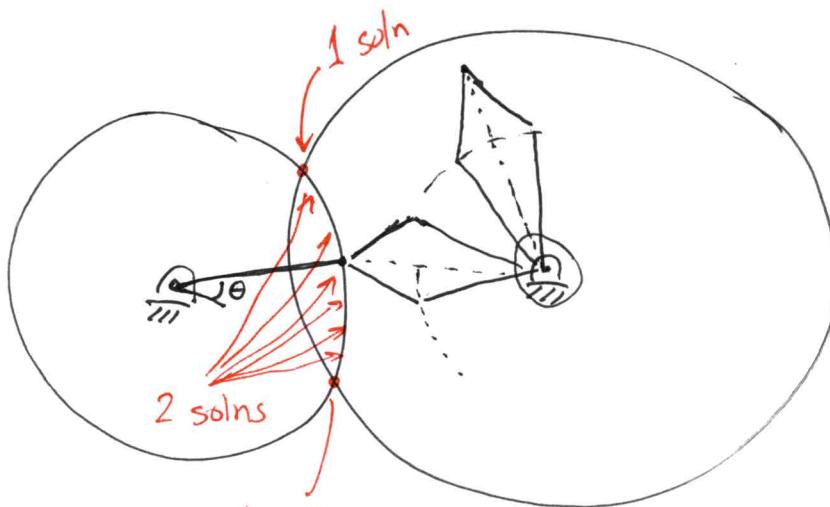
$$C = I \times I \times I = I^3$$

Now close  
the loop



What's a good parameterization?  
Now C-space is one-dimensional, not 3D.

# Global structure of C-space for a planar four-bar.

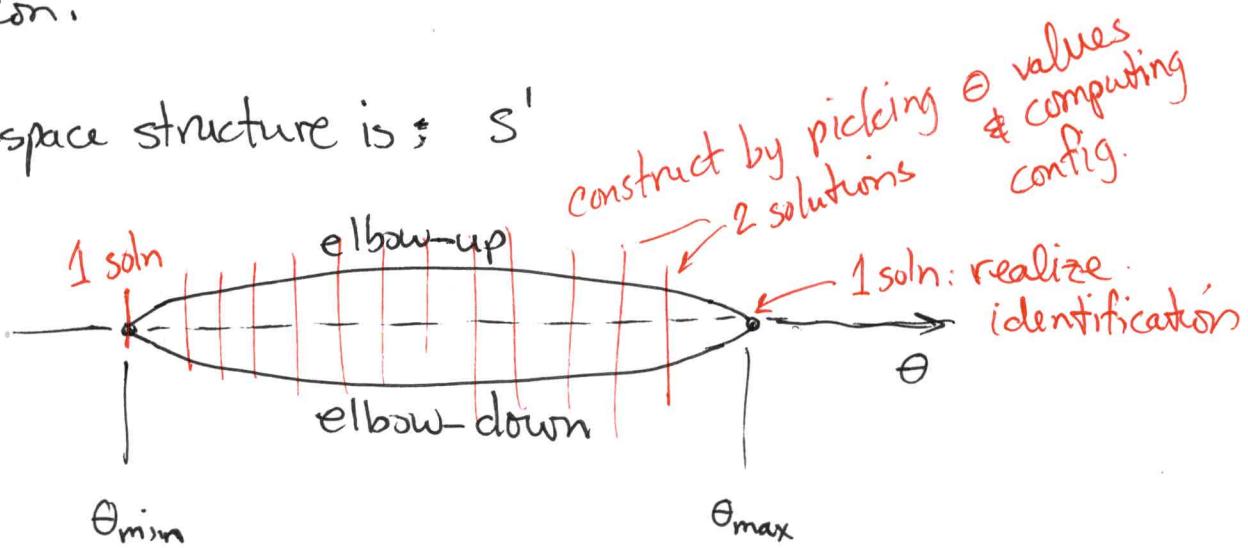


As  $\theta$  changes  
the 2R on the  
right always has  
2 solns; elbow-up  
and elbow-down.

↑ This circle is in  
some sense critical  
to C-space structure.

Until it gets to an extreme position off its range  
of motion. Then elbow-up soln  $\equiv$  elbow-down  
solution.

So Cspace structure is; S'



2/11/18

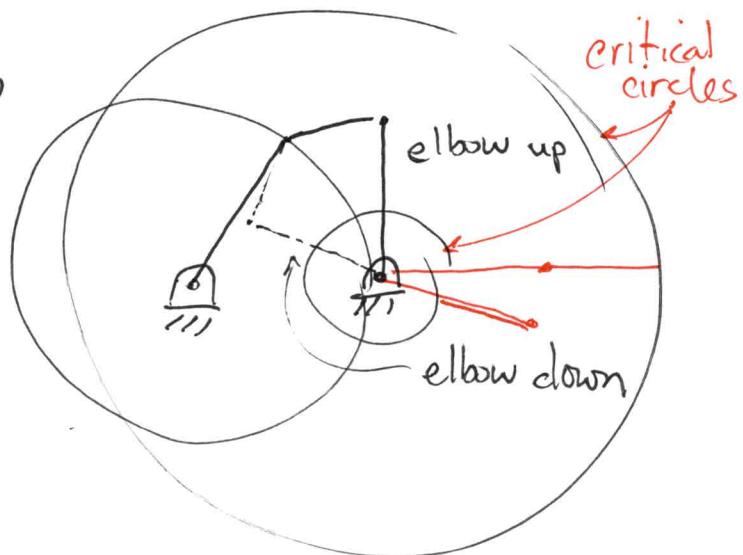
(6)

This knowledge allows your algorithm to generate motions that switch from elbow-down to elbow-up and vice versa as needed.

What's the C-space?

Two disconnected circles

$$C = S'_* \sqcup S'$$



Show slide 18 from ClosedChains.pptx

What is C-space for a 5-bar?

In this case, you get a triple torus; 2D surface with 3 holes.

